



OPTIMAL DESIGN PSS-PID CONTROL ON SINGLE MACHINE INFINITE BUS USING ANT COLONY OPTIMIZATION

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Abstract

Optimization of the controller in a generator can improve system performance. The right parameter optimization is needed to get the optimal performance from the controller. The application of the artificial intelligence method as a parameter optimization method is proposed in this study. By using the smart method based on Ant Colony, the optimal PSS-PID parameters are obtained. With optimal tuning, the system gets optimal Single Machine Infinite Bus (SMIB) system frequency and rotor angle response, indicated by the minimum overshoot system response. The SMIB system's stability will be tested. A case study of adding and reducing loads is used, with the proposed control method PSS-PID being optimized using Ant Colony. Based on the analysis using the proposed PSS-PID control, we get the minimum overshoot for the frequency response and rotor angle of the SMIB system. When the load changes at 20 seconds, using the PSS-PID control scheme, the minimum overshoot is $-4.316e-06$ to $7.598e-05$ pu with a settling time of 22.01s. For the rotor angle overshoot response, using the PSS-PID control scheme, the minimum overshoot is -0.01113 to -0.009669 pu with a settling time of 22.36s.

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INTRODUCTION

In the dynamic stability analysis, because the governor response is slow, the torque is neglected. With the slow governor response compared to the excitation system response, the excitation system regulates the controller. In its application, the addition of an excitation amplifier circuit is not optimal to stabilize the system, especially Low Frequency Oscillation 0.2 - 2.0 Hz [1].

Low frequencies can turn into oscillations between areas, so additional controllers such as Power System Stabilizer and PID are needed. PSS is additional control equipment on generator excitation that is used to provide additional attenuation to generator excitation [2][3]. PID is an additional control that functions to reduce local or global oscillations in the generator and respond to deviations that occur at predetermined variable values [4][5]. It requires

precisely adjusting the PSS and PID to reduce oscillation and properly stabilize the system optimally to get maximum results. Controller parameters are optimized using smart methods [6][7].

The Ant Colony Optimization (ACO) algorithm is a Swarm Intelligence group that can solve optimization problems. ACO adopts group or insect swarming behavior [8][9]. In several previous studies, the ACO method was also used for the optimization of PID controllers [10][11]. Several other studies related to the application of smart methods can improve generator performance, such as firefly method [2], bat algorithm [12, 13, 14], flower pollination [15], imperialist competitive [4], and cuckoo search [3][5].

Optimal parameter tuning of the controller will be very influential in stabilizing the system. However, the range of equipment parameters is

very diverse and broad, so to get the parameter values quickly, an optimization method using ACO is used. The response value is known by analyzing the overshoot and settling time values, while the objective function minimizes Integral Time Absolute Error (ITAE) [16][17].

The case study used in this research is the Single Machine Infinite Bus (SMIB) system. SMIB is an electric power subsystem consisting of one or more generators that are connected to an infinite bus [18]. Then analyze the simulation results by comparing the simulation system results without control, SMIB with PID, SMIB with PSS, and the proposed method of SMIB with PSS-PID with ACO. In this study, the authors implemented an Ant Colony-based intelligent method to solve the optimization problem of determining the PSS-PID parameters on the SMIB system.

METHOD

There are several steps in conducting research. The research begins with the study of literature, analysis, and conclusions.

Data Analysis

The case study used is a single machine infinite bus (SMIB) system regarding previous research modeling [19]. Some stages of analysis are, modelling the synchronous machine system, modelling the PSS-PID using Simulink, entering the system data, designing the ACO, plotting the proposed method results, and comparing it with the other control schemes.

Machine Model

The synchronous machine model is modeled in linear modelling, as shown in Figure 1 [19].

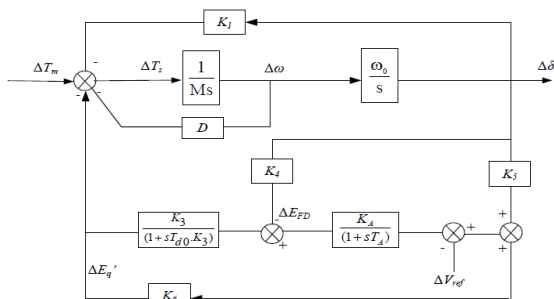


Figure 1. Synchronous Linear Machine Model

Where:

- K_1 - K_6 = Constant
- E_{FD} = Magnetic field flux
- T_m = Turbine mechanical torque (N.m)
- T_e = Rotor electric torque (N.m)
- T_a = Acceleration of torque (N.m)

- T = Time (detik)
- δ_m = Rotor mechanical angle (rad-mechanical)
- D = Engine damping coefficient
- E_q' = Stator field flux
- $\Delta\delta$ = Change in engine angle
- M = Momentum
- $\Delta\omega$ = Speed

Exciter Model

Excitation equipment in the system is used to control the generator output variable [2]. This study's excitation modeling refers to the IEEE modeling shown in Figure 2 [19].

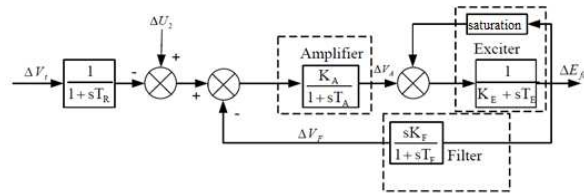


Figure 2. Excitation Model

Where:

- K_A = Amplifier gain constant
- K_F = Filter gain constant
- K_E = Exciter gain constant
- T_A = Amplifier response time
- T_E = Exciter response time
- T_F = Filter response time
- ΔU_2 = Change of an engine control signal

Governor Model

Governor is a controller used to regulate the mechanical torque value of T_m , which is input from the generator [19]. Governor modeling is shown in Figure 3.

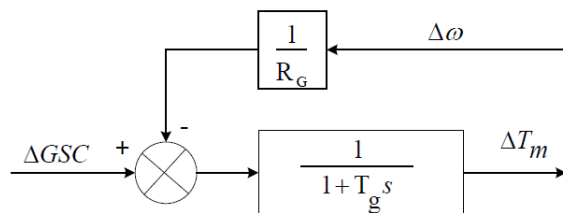


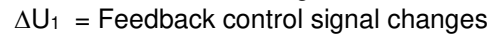
Figure 3. Governor Model

Where:

- K_g = Constant gain = $1/R_g$
- T_g = Constant governor time
- R_g = Governor's groove constant
- ΔGSC = Governor Speed Changer

Turbine Model

The turbine model used is a steam turbine power plant model [20]. The model is shown in Figure 4.



Model is shown as the Single Machine Infinite Bus (SMIB) model in [Figure 5](#) [14].

pheromones that other Ants leave behind. The ant then selects city j on the candidate list following the transition rule in (1). P is the Ant's movement from i to j .

$$j = \begin{cases} \underset{u \in J_i^k}{\operatorname{argmax}} \{ [\tau_{iu}(t)] [\eta_{iu}(t)]^\beta \} & , \text{if } q \leq q_0 \\ J & , \text{the other} \end{cases} \quad (1)$$

$$P_{ij}^k = \frac{[\tau_{iu}(t)] [\eta_{iu}(t)]^\beta}{\sum_{l \in J_i^k} [\tau_{il}(t)] [\eta_{il}(t)]^\beta} \quad (2)$$

Where:

τ = Pheromones

η = the distance between two nodes

q = A random variable $[0,1]$

q_0 = Parameters that can be set at intervals $[0,1]$

J = A list of candidates

Ant Colony Optimization Parameter

Some parameters used in the ACO method in this thesis are as follows, the number of ants = 10, the maximum iteration = 50, and the Pheromone Resistance (α) = 0.9

Tuning PSS-PID Control with Ant Colony

The objective function used in this study is to optimize the Integral Time Absolute Error.

$$ITAE = \int_0^t |\Delta \omega(t)| dt \quad (3)$$

Where ω is a speed that is tested for stability. The PSS-PID parameters tuned by ACO are K_p , K_i , K_d , K_{pss} , T_1 , T_2 , T_3 , T_4 .

The algorithm design is mentioned in Table 1, to run the Ant Colony optimization. The Ant Colony algorithm was created using the MATLAB-Simulink software.

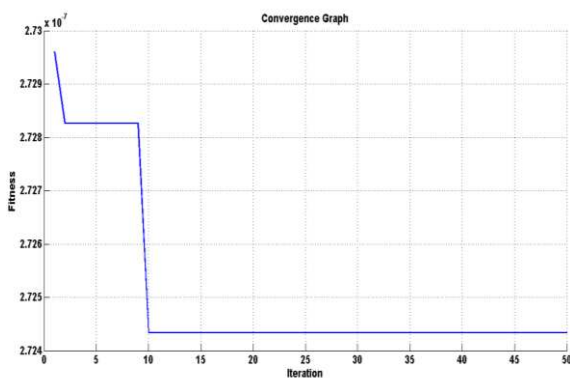


Figure 7. Convergence Graph

Table 1. Ant Colony Parameter

Parameters	Values
Number of Ants (n)	8
Max Iteration (It)	50
Pheromone (α)	0.9
Beta (β)	2

After entering several parameters in Table 1, the Ant Colony algorithm is run to optimize the PSS-PID value. The exact value will greatly affect the SMIB response performance designed in this study. The Ant Colony algorithm requires a calculation process to get the optimal value. Figure 7 shows a graph of PID convergence optimization using the Ant Colony algorithm. Convergence is the value of the fitness function, which describes the optimal criteria for an optimization problem.

Figure 7 displays the convergence graph of PSS-PID value optimization using Ant Colony. The Ant Colony algorithm does not take a long time to perform the optimization process. In the 10th iteration, the algorithm has found the optimal PSS and PID values with a minimum fitness value of $2.724e-07$.

The ACO results obtained a fitness function value of $2.724e-07$, with iteration 50 times convergent in the 10th iteration, the best value is the best Ant Colony known as the PID parameter optimization results, namely K_p , K_i , K_d , K_{pss} , T_1 , T_2 , T_3 , T_4 . Table 2 shows the limits and values of the PSS-PID parameter optimization results set by the Ant Colony.

Table 2. Limits and ACO Optimization Results

Parameter	Limits		Results
	Lower	Upper	
K_p	0	10	5.0311
K_i	0	100	1.1755
K_d	0	10	1.0043
K_{pss}	0	10	64.1961
T_1	0	10	0.5266
T_2	0	10	0.2317
T_3	0	10	1.0971
T_4	0	10	5.4010

As a comparison, several control schemes are used, namely the combination of PID, PSS and PSS-PID. In principle, the Ant Colony algorithm looks for food sources based on pheromones, which then in groups will follow the trail with the largest pheromone [10]. With this principle, the algorithm will look for the most optimal parameters to be filled in the PID parameters, so that optimal control is obtained at the SMIB. The flow chart in this study is shown in Figure 8.

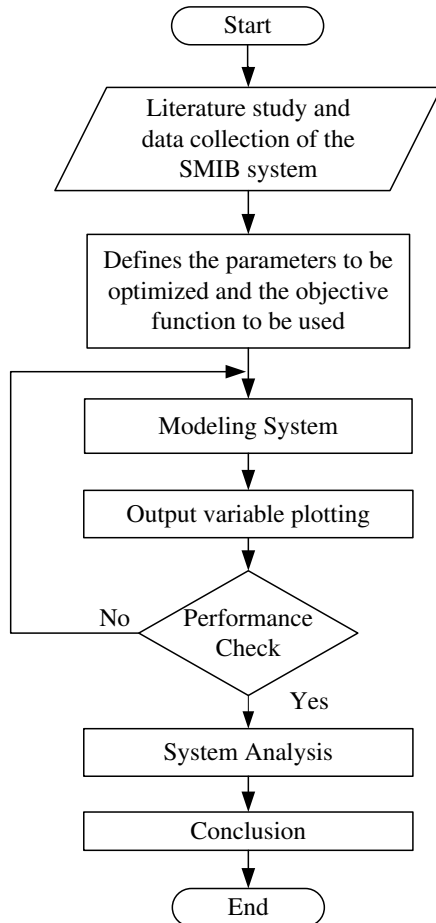


Figure 8. Research Flowchart

RESULTS AND DISCUSSION

The system analysis is performed, namely the analysis of the system frequency and SMIB rotor angle. The analysis was carried out using several control methods, such as the uncontrolled system, SMIB-PID, SMIB-PSS, and PSS-PID SMIB. PSS and PID parameters are simulated using the Ant Colony Optimization algorithm. The SMIB system is given a disturbance in the form of load changes to test the system's stability.

SMIB Frequency Response

The first analysis begins by reviewing the frequency stability response of the SMIB system. The simulation results are shown in Figure 9. Figure 9 display the simulation results of the SMIB frequency response with several control methods.

From the SMIB system's simulation results, a load change disturbance of 0.01 pu is given in the second, then the load shedding that occurs in the 20th second is 0.005 pu. At the first load change, the load increase increases the condition where the electric power is not the same as the mechanical power (P_m). In this

condition, $P_e > P_m$, the electric torque and mechanical torque are not balanced. This condition causes the electric frequency (Δf) to change as well. During this instability, the rotor rotational speed ($\Delta \omega$) becomes out of sync. In this condition, the frequency response graph drops before returning to a steady state. The control system function is then required to return to steady state. The characteristics of the overshoot response in this condition are shown in Table 3.

Table 3. Frequency Deviation

Deviation	Overshoot (pu)
SMIB	-0.0002409 & 0.0001865
SMIB-PID	-0.0002069 & 0.0002129
SMIB-PSS	-0.0001748 & 1.787e-05
SMIB-PSS-PID	-0.0001533 & 7.662e-05

Table 3 shows the overshoot system's characteristics when the load changes at the 1st second in the form of additional loads. The uncontrolled SMIB system has an overshoot of -0.0002409 to 0.0001873 pu with a turnaround time of 15.09s. With PID control, the SMIB system gets an overshoot of -0.0002069 to 0.000131 pu with a settling time of 11.78s. With PSS control, the SMIB system obtained an overshoot of -0.0001748 to 8,743e-05 pu with a settling time of 2,334s. With the proposed method using PSS-PID, the smallest overshoot is obtained from -0.0001533 to 7.662e-05 pu with a settling time of 3.334s.

Then in the next load change in the form of a load reduction which causes the electric power (P_e) to change. In this condition, the electric power is not the same as the mechanical power (P_m) $P_e < P_m$, so that the electric torque and mechanical torque are not balanced. This condition causes the electric frequency (Δf) to change as well. During this instability, the rotor rotational speed ($\Delta \omega$) becomes out of sync. In this condition, the frequency response graph rises before returning to a steady state. The control system function is then required to return to steady state. The characteristics of the overshoot response in this condition are shown in Table 4. Figure 9 is a graph of the system's electrical frequency response (Δf).

Table 4. Frequency Deviation

Deviation	Overshoot (pu)
SMIB	-9.314e-05 & 0.0001203
SMIB-PID	-6.515e-05 & 0.000131
SMIB-PSS	-9.369e-06 & 8.743e-05
SMIB-PSS-PID	-4.316e-06 & 7.598e-05

Table 4 displays the overshoot method's features when the load shifts in the form of a load reduction at the 20th second. With a turnaround period of 32.17s, the uncontrolled SMIB device surpassed -9.314×10^{-5} to 0.0001203 pu. The SMIB system obtained an overshoot of -6.515×10^{-5} to 0.000131 pu with PID control with a settling time of 26.54s. The SMIB network obtained an overshoot with PSS control.

Rotor Angle Response

The subsequent analysis looked at the performance of the SMIB rotor response angle by installing a PSS-PID control. In this study, the test for SMIB was given in the form of a change of 0.05 pu at 1 s. The change in question is an increase and an increase in expenses. An increase in load will cause changes in electrical power also to increase. Suppose that the generator's mechanical power is greater than the electric power; it can cause acceleration in the rotor. In this case, the rotor acceleration will also affect the change in rotor angle. The rotor angle response will be reduced or negative from the conditions before the disturbance, shown in Figure 10. The response of the generator rotor angle for each method is shown in Table 5.

Table 5. Rotor Angle Deviation

Deviation	Overshoot (pu)
SMIB	-0.03651 & -0.00874
SMIB-PID	-0.01306 & -0.03332
SMIB-PSS	-0.01888 & -0.02264
SMIB-PSS-PID	-0.02093 & -0.02197

Table 5 shows the system overshoot characteristics for the load change conditions at the 1st second. The uncontrolled SMIB system has an overshoot from -0.03651 to -0.00874 pu

with a turnaround time of 18.88s. With PID control, the SMIB system obtained an overshoot of -0.01306 to -0.03332 pu with a settling time of 11.59s. With PSS control, the SMIB system gets an overshoot of -0.01888 to -0.02264 pu with a settling time of 5.026s. With the proposed method using PSS-PID, the lowest overshoot is -0.02093 to -0.02197 pu with a settling time of 3.283 pu.

Then in the next load change in the form of a load reduction at the 20th second. In this condition, the generator's mechanical power is less than the electric power, causing a slowdown in the rotor. This situation occurs because the magnetic coupling will push the stator field with the rotor field to increase the generator rotor angle, as shown in Figure 10. The characteristics of the overshoot system in this condition are shown in Table 6.

Table 6 displays the features of the overshoot system for load change conditions at the 20th second. The uncontrolled SMIB system goes beyond -0.01651 to -0.002530 pu with a completion time of 36.47 seconds. The SMIB system obtained an overshoot of -0.01437 to -0.003934 pu with PID control with a settling time of 129.55s. The SMIB system gets an overshoot of -0.01145 to -0.009567 pu with PSS control, with a settling time of 23.54s. The smallest overshoot is -0.01113 to -0.009669 pu, with a settling time of 22.36s, with the proposed approach using PSS-PID.

Table 6. Rotor Angle Deviation

Deviation	Overshoot (pu)
SMIB	-0.01651 & -0.002530
SMIB-PID	-0.01437 & -0.003934
SMIB-PSS	-0.01145 & -0.009567
SMIB-PSS-PID	-0.01113 & -0.009669

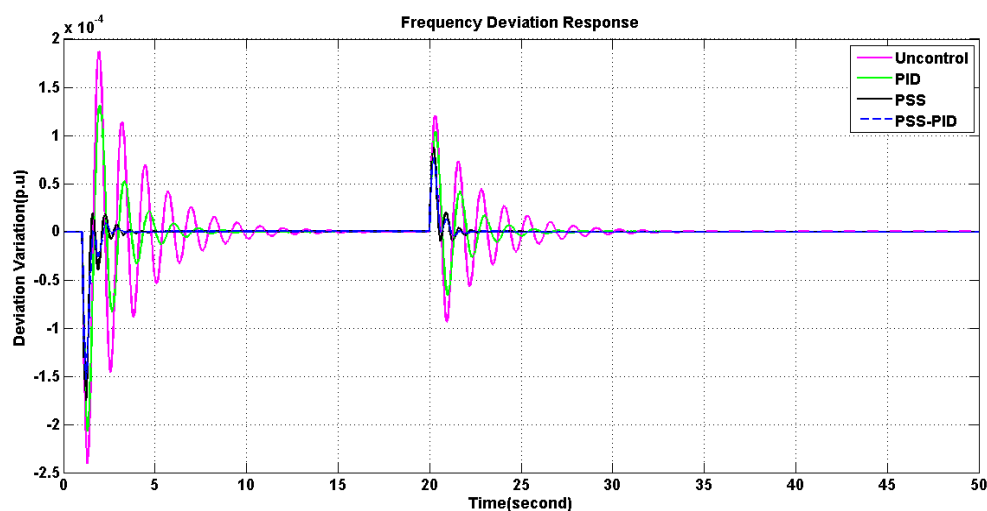


Figure 9. SMIB Frequency Response

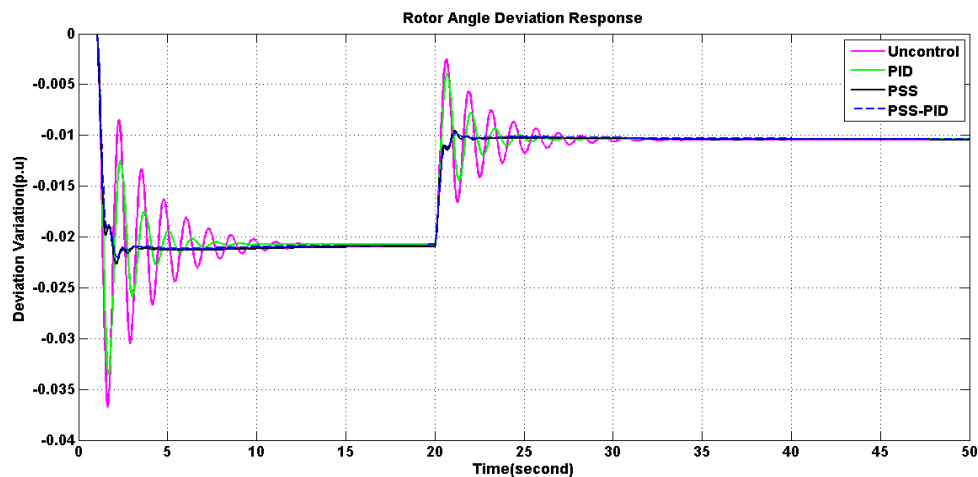


Figure 10. SMIB Rotor Angle Response

CONCLUSION

According to the comparative results, the optimal parameters of PSS-PID tuned by using ACO are $K_p = 5.0311$, $K_i = 1.1755$, $K_d = 1.0043$, $K_{pss} = 64.1961$, $T_1 = 0.5266$, $T_2 = 0.2317$, $T_3 = 1.0971$, $T_4 = 5.4010$. A perfect SMIB frequency response is obtained with optimal tuning compared with an uncontrolled system, SMIB-PID and SMIB-PSS. The condition is indicated by an improved system response, where the controller can provide stability—increased system performance with minimum overshoot oscillations and faster settling times.

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