Journal of Renewable Energy, Electrical, and Computer Engineering

Volume 5, Number 1, March 2025. 45-50 eISSN 2776-0049

Research Original Article

DOI: https://doi.org/10.29103/jreece.v5i1.15014

Calculation of the Effect of Substation Configuration on the Resistance Value of the Grounding System

Ayu Fitriani^{⊠1}, Jhoni Hidayat², Joel Panjaitan³, Syofyan Anwar Syahputra⁴, Mili Alfisari⁵

^{1,2}Universitas Tjut Nyak Dhien, Teknik Elektro, Medan Helvetia, Kota Medan, 20123, Sumatera Utara, <u>ayufitriani2796@gmail.com</u>

^{3,4}Akademi Teknik Deli Serdang, Teknik Elektro, Jln. Medan, Lubuk Pakam, 123456, Sumatera Utara, joel.pandjaitan@gmail.com

⁵STIMIK Kaputama, Jl. Veteran No.4A, Tangsi, Kec. Binjai Kota, Kota Binjai, Sumatera Utara, milli.fhisya@gmail.com

[™]Corresponding Author: <u>ayufitriani2796@gmail.com</u> | **Phone: +6285360988947**

Received: January 23, 2024 Revision: January 15, 2025 Accepted: March 10, 2025

Abstract

Generally, the configuration of the substation grounding system is in the form of a grid or mesh, where several conductor rods are installed vertically and horizontally or combined with conductor rods planted deep in the ground from each point or not. The substation configuration is very complex because of the many variables used in accordance with IEEE Standard 80-2013. This variable also influences the allowable and actual magnitude of the step voltage and touch voltage. The substation grounding system configuration can be designed in several shapes including rectangular, square, L-shaped and T-shaped. The parameters used are an area of 70 m x 70 m, a conductor rod depth of 0.5 meters with a total conductor length for a rectangle of 1540 meters without rods, an L-Shaped shape of 1755 meters and a T-Shaped shape of 3857 meters. The results obtained by the resistance of the grounding system without rods in the T-Shaped configuration were 2.39 Ω . For the resistance results, the grounding system uses a rod with the same area and a conductor length of 3917 meters with a resistance value of 2.39 Ω in the T-shape configuration. The results of the resistance values obtained with various forms of grounding system configurations and varying conductor lengths are still safe and below the threshold or standard of the grid grounding system.

Keywords: Resistance, Rectangular, L-Shaped, T-Shaped

Introduction

There are 2 (two) factors that cause disturbances at substations that cannot be denied, including internal disturbances and external disturbances (Amadi, 2017), (Ibrahim, 2011), (Pickett et al., 2015), (Zimba et al., 2017). Internal factors include technician errors, installation errors and equipment damage. External disturbances are caused by natural factors, for example landslides, floods, lightning strikes, strong winds, earthquakes and others (Jose & others, 2015), (Paul & others, 2020), (Shroder, 2021), (Keller & DeVecchio, 2019), (Smith et al., 2023). This causes the installation of protective equipment to secure the equipment at the substation (Putra et al., 2023). The substation is the link between the transmission line and the distribution network. The configuration or construction of the substation is also an important factor in meeting the requirements in accordance with the design standards for a substation (Hu et al., 2021), (Huang et al., 2016), (Altaher, 2018), (Krieg, 2019). Generally, the configuration of the substation grounding system is in the form of a grid or mesh, where several conductor rods are installed vertically and horizontally or combined with conductor rods planted deep in the ground from each point or not (Uzunlar & Kalenderli, 2009), (Adebayo & Ujam, 2023). The combination of these conductor rods can reduce the value of grounding resistance to as little as possible. The best ground resistance value is below 5 ohms or preferably 1 ohm (Cheema et al., 2015). The substation configuration is very complex because of the many variables used in accordance with IEEE Standard 80-2013 (Hardi et al., 2021). This variable also influences the allowable and actual magnitude of the step voltage and touch voltage (Kostić & Raičević, 2016). The substation grounding system configuration can be designed in several shapes including rectangular, square, L-Shaped and T-Shaped (IEEE 80-2000). Each form of grounding configuration is completed using the parameters contained in the IEEE 80-2013 standard (Gouda, 2024).

Literature Review

Based on the results of a series of field tests conducted by measuring ground rod electrodes in different types of soil at low soil depths on podzolic soil types with yellowish clay soil characteristics and red pebbles having a relatively high soil resistivity, podzolic soil resistivity values are a combination of wet clay and sand. Hence, it assumes 150 Ω .m. This is consistent with the significant grounding resistance seen when utilizing rod electrodes. The best grounding resistance is shown when using a galvanized iron type grounding rod electrode, particularly at a depth of 2 meters in the ground, where the resistance value using a galvanized type rod electrode is 10% to 20% lower than when using an iron type rod

electrode or a copper-coated iron type, indicating that the grounding resistance is not as good when using an iron type rod electrode or a copper-coated iron type (Uzunlar & Kalenderli, 2009). Its maximum allowable value varies from 10Ω (or lower) for lightning protection to 0.1Ω for sites where protective devices must operate very quickly. The grounding grid design is an important factor in a substation for fulfilling standard requirements formulated by IEEE Std. 80. Commonly, substation grounding is a grid configuration or combination of grid and rod. This study is designing a substation economically by considering the length of the rod conductor used. Some grid configuration models were used for analyzing viz. rectangular shape, T-shape, and L-shape. The models were compared with the existing design in the Galang substation to find the minimum conductor length (Hardi et al., 2021).

Materials & Methods

The grid grounding system used in this research is a grounding system configuration in rectangular shape, L-shaped shape, and T-shaped shape using rods and without rods. The rod grounding system uses 20 conductor rods that are plugged into the ground. Other parameters used are the grounding resistance value of 400 ohms, the depth of the conductor rod is 0.5 meters with a total conductor length for a rectangle of 1540 meters without the rod, 1690 with the rod, the L-Shaped shape is 1755 meters and the T-shaped shape is 3857 meters, can be shown in the flowchart below:

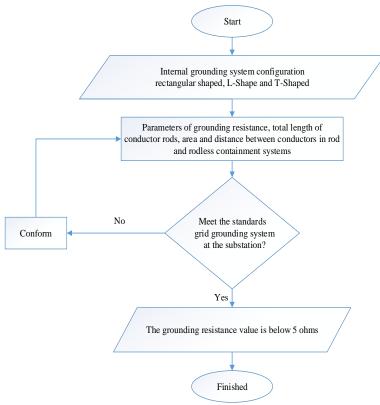


Figure 1. Research Flowchart

Results and Discussion

Configure the Grounding System in a Square Shape

The assumption for the grid grounding area without rods is $70 \text{ m} \times 70 \text{ m}$ with the same distance between conductors, namely D = 7 meters, with a depth of embedding the conductor rods, namely h = 0.5 meters, which can be shown in Figure 2 below:

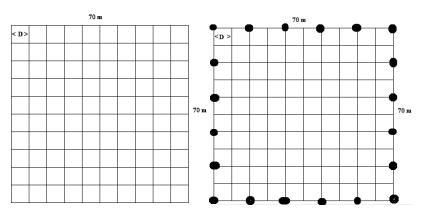


Figure 2. Grounding System Configuration in Square Shape Without Rod and With Rod

Determining the resistance of grounding without rods using the equation for the total length of the grounding rods $L_T = 1540$ m and area A = 4900 m² is:

$$R_G = \rho \left[\frac{1}{Lt} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h\sqrt{\frac{20}{A}}} \right)$$

$$R_G = 400 \left[\frac{1}{1540} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5 \sqrt{\frac{20}{4900}}} \right) = 2,78 \,\Omega$$

The assumption for determining the grounding resistance with rods is 20 rods with a rod length of 7.5 meters. Determining the grounding system with rods uses the equation for the total length of the grounding rods L_T = 1540 + 20 + 7.5 = 1690 m² and area A = 4900 m²,

$$R_G = \rho \left[\frac{1}{Lt} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h\sqrt{\frac{20}{A}}} \right)$$

$$R_G = 400 \left[\frac{1}{1690} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5 \sqrt{\frac{20}{14000}}} \right) = 2,75 \,\Omega$$

Grounding System Configuration in L-Shaped Form

Assumption for the grid grounding area without rods is 70 m x 70 m with the same distance between conductors, namely D = 7 meters, with a depth of embedding the conductor rods, namely h = 0.5 meters, and the overall length of the conductor rods, namely $L^T = 1575$ m, can be shown in Figure 3 below:

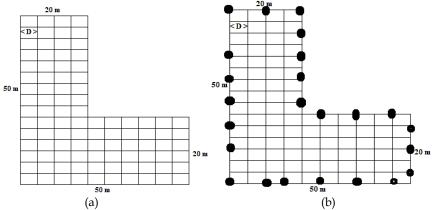


Figure 3. Grounding System Configuration in L-Shaped Form Without Rod and With Rod

Determining an L-Shaped grounding system without rods using the equation for the total length of the grounding rods L_T = 1575 m and area A = 4900 m2 is:

$$R_{G} = \rho \left[\frac{1}{\text{Lt}} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h \sqrt{\frac{20}{A}}} \right)$$

$$R_{G} = 400 \left[\frac{1}{1575} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5 \sqrt{\frac{20}{4900}}} \right) = 2,67 \ \Omega$$

Determining an L-Shaped grounding system without rods using the equation for the total length of the grounding rods LT = 1575 m + (24) (7.5 m) = 1755 m and area A = 4900 m2 is:

$$R_G = \rho \left[\frac{1}{Lt} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h\sqrt{\frac{20}{A}}} \right)$$

$$R_G = 400 \left[\frac{1}{1755} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5\sqrt{\frac{20}{4900}}} \right) = 2.64 \Omega$$

Grounding System Configuration in T-Shaped Form

The assumption is that the grid grounding area without rods is 70 m x 70 m with the same distance between

conductors, namely D = 7 meters, with the depth of embedding the conductor rods, namely h = 0.5 meters, and the overall length of the conductor rods, namely $L_T = 3857$ m without rods, can be shown in Figure 4 below:

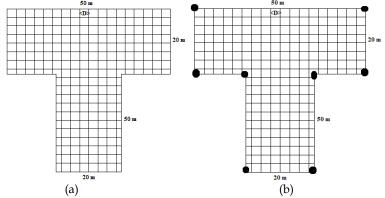


Figure 4. Grounding System Configuration in T-Shaped Form Without Rod and With Rod

Determining a T-Shaped grounding system without rods using the equation for the total length of the grounding rods L_T = 3857 m and area A = 4900 m2 is:

$$R_G = \rho \left[\frac{1}{Lt} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h \sqrt{\frac{20}{A}}} \right)$$

$$R_G = 400 \left[\frac{1}{3857} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5 \sqrt{\frac{20}{A900}}} \right) = 2,39 \,\Omega$$

Determine the L-Shaped grounding system with rods using the equation for the total length of the grounding rods L_T = 3857 m + (8) (7.5 m) = 3917 m and area A = 4900 m2 is:

$$R_G = \rho \left[\frac{1}{Lt} \right] + \frac{1}{\sqrt{20A}} \left(1 + \frac{1}{1 + h\sqrt{\frac{20}{A}}} \right)$$

$$R_G = 400 \left[\frac{1}{3917} \right] + \frac{1}{\sqrt{20.4900}} \left(1 + \frac{1}{1 + 0.5\sqrt{\frac{20}{4900}}} \right) = 2,39 \ \Omega$$

The grounding resistance value for each type of configuration can be shown in Table 1 below.

Table 1. Resistance Calculation Results for a Grid Grounding System Without Rods

Configuration Form	Area (m²)		Conductor	Resitance
	X	Y	length (m)	Grid (Ω)
Rectangle	70	70	1540	2,78
L-Shaped	70	70	1575	2,67
T-Shaped	70	70	3857	2,39

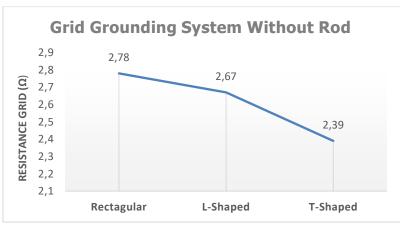


Figure 5. Graph of a Grid Grounding System Without Rods

The results of the calculation of the resistance of the grounding system using rods are shown in Table 2 below.

Table 2. Results of Grid Grounding System Resistance Calculations Using Rods

Configuration		Area (n	1 ²)	Conductor length (m)	Resitance Grid (Ω)
Form	X	Y	Rod		
Rectangle	70	70	20	1650	2,75
L-Shape	70	70	24	1755	2,64
T-Shape	70	70	8	3917	2,39

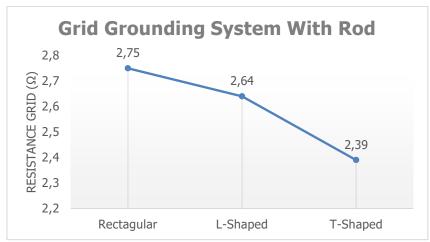


Figure 6. Graph of a Grid Grounding System With Rods

From graph 5 and graph 6 it shows that with the same area, the length of the installed conductor varies with different grounding configurations, the smallest grounding resistance results are found in the grounding system with a T-shaped configuration, namely 2.39 Ω . The results of grid grounding resistance calculations using rods are also in the T-shaped configuration with the same value, namely 2.39 Ω .

Conclusions

From the results of the calculation of the resistance value of the grounding system without rods and using rods in a grounding system configuration in square, L-Shaped and T-Shaped with a resistance value of $400\,\Omega$, with rods installed in various ways, the results of the resistance of the grounding system without rods are obtained. In the T-Shaped configuration with an area of $70~m\times70~m$, the conductor length is 3857~m eters with a resistance value of $2.39\,\Omega$. For the resistance results, the grounding system uses a rod with the same area and a conductor length of 3917~m eters with a resistance value of $2.39\,\Omega$ in the T-shape configuration. The results of the resistance values obtained with various forms of grounding system configurations and varying conductor lengths are still safe and below the threshold or standard of the grid grounding system.

Acknowledgments

Thank you to all my fellow lecturers who always give encouragement to writers, as well as appreciation for myself who never gets tired of always learning better in writing scientific journals, and don't forget to my parents who always faithfully pray for me every step of change and progress in achieving success.

References

Adebayo, A. D., & Ujam, C. J. (2023). Analysis of electrical grounding design of substation and lines. *International Journal of Scholarly Research in Engineering and Technology*, 2(1), 31–40.

Altaher, A. (2018). *Implementation of a dependability framework for smart substation automation systems: application to electric energy distribution*. Université Grenoble Alpes.

Amadi, H. N. (2017). Design of grounding system for AC substations with critical consideration of the mesh, touch and step potentials. *European Journal of Engineering and Technology Vol*, 5(4).

Cheema, M. U., Cheema, M., Bashir, A., & Aslam, M. U. (2015). A comparison of ground grid mesh design and optimization for 500KV substation using IEEE 80-2000 and finite element methods. *Electrical and Electronics Engineering: An International Journal (ELELIJ)*, 4(1), 131–146.

Gouda, O. E.-S. (2024). Step and Touch Voltages and Grounding Potential Rise (IEEE and IEC). In *Performance of Grounding Grids at Faulty and Lightning Strokes Conditions* (pp. 221–294). IGI Global.

Hardi, S., Andira, R., Nisja, I., Octrialdi, B., & Pinem, M. (2021). Economic design of substation grounding grid using etap software: a case study of 2 x 500 mva galang substation. *Journal of Physics: Conference Series*, 1811(1), 12055.

Hu, H., Fang, M., Hu, F., Zeng, S., & Deng, X. (2021). A new design of substation grounding based on electrolytic cathodic protection and on transfer corrosion current. *Electric Power Systems Research*, 195, 107174.

Huang, Q., Jing, S., Li, J., Cai, D., Wu, J., & Zhen, W. (2016). Smart substation: State of the art and future development. *IEEE Transactions on Power Delivery*, 32(2), 1098–1105.

- Ibrahim, M. A. (2011). *Disturbance analysis for power systems*. John Wiley \& Sons.
- Jose, S., & others. (2015). Practical Approach on Lightning and Grounding Protection System. *International Journal of Engineering Research*, 4(4), 192–196.
- Keller, E. A., & DeVecchio, D. E. (2019). Natural hazards: earth's processes as hazards, disasters, and catastrophes. Routledge.
- Kostić, V. I., & Raičević, N. B. (2016). An alternative approach for touch and step voltages measurement in high-voltage substations. *Electric Power Systems Research*, 130, 59–66.
- Krieg, T. (2019). Substations. In Springer Handbook of Power Systems (pp. 867–934). Springer.
- Paul, V. K., & others. (2020). *Understanding Vulnerability and Resilience of Critical Infrastructure in Extreme Weather Events*. New Delhi, India: School of Planning and Architecture, New Delhi.
- Pickett, B., Elkin, P., Benner, C., Carroll, P., Hataway, G., Houser, K., Liao, Y., Martin, A., Mulawarman, A., Mysore, P., & others. (2015). Reducing outages through improved protection, monitoring, diagnostics, and autorestoration in transmission substations (69 kV and above). *IEEE Transactions on Power Delivery*, 31(3), 1327–1334.
- Putra, D. E., Pardede, G. P. V, Kurniawan, F., Saputra, M. W., Sinaga, R., Rahmanda, A., Rudini, B., Putra, R. E., & Salis, M. W. (2023). Comparison of grounding resistance using grounding rod electrodes with different fault current types in podzolic soil at Prabumulih Substation. *Journal of Renewable Energy, Electrical, and Computer Engineering*, 3(1), 19–25.
- Shroder, J. F. (2021). Landslide hazards, risks, and disasters. Elsevier.
- Smith, K., Fearnley, C. J., Dixon, D., Bird, D. K., & Kelman, I. (2023). *Environmental hazards: assessing risk and reducing disaster*. Routledge.
- Uzunlar, F. B., & Kalenderli, Ö. (2009). Three dimensional grounding grid design. 2009 International Conference on Electrical and Electronics Engineering-ELECO 2009, I--139.
- Zimba, S. K., Nyamutswa, I., & Chikova, A. (2017). Islanding power systems to minimize impact of system disturbances in Southern African Power Pool. 2017 IEEE AFRICON, 1107–1112.